Proceedings of the Institution of Mechanical Engineers, Part H: Journal of Engineering in Medicine

Knee joint forces: prediction, measurement, and significance

Darryl D D'Lima, Benjamin J Fregly, Shantanu Patil, Nikolai Steklov and Clifford W Colwell, Jr

The online version of this article can be found at:

Published by:

$SAGE

On behalf of:

Institution of MECHANICAL ENGINEERS

Institution of Mechanical Engineers

>> Version of Record - Jan 25, 2012

What is This?

Knee joint forces: prediction, measurement, and significance

Darryl D D'Lima[1], Benjamin J Fregly[2], Shantanu Patil[1], Nikolai Steklov[1] and Clifford W Colwell Jr[1]

Abstract

Knee forces are highly significant in osteoarthritis and in the survival and function of knee arthroplasty. A large number of studies have attempted to estimate forces around the knee during various activities. Several approaches have been used to relate knee kinematics and external forces to internal joint contact forces, the most popular being inverse dynamics, forward dynamics, and static body analyses. Knee forces have also been measured in vivo after knee arthroplasty, which serves as valuable validation of computational predictions. This review summarizes the results of published studies that measured knee forces for various activities. The efficacy of various methods to alter knee force distribution, such as gait modification, orthotics, walking aids, and custom treadmills are analyzed. Current gaps in our knowledge are identified and directions for future research in this area are outlined.

Introduction

The knee is an important load-bearing joint, which is distinct from the other major load-bearing joints in that soft tissues rather than articular shape are the major stabilizing factors.[1] Other important differences are the division of the joint into three compartments (two tibiofemoral and one patellofemoral) and the presence of menisci, which contribute significantly in the transfer of contact stresses from one articular surface to another.[2] While the patellofemoral joint is an important component of the knee, tibiofemoral forces are the primary focus of this review.

Knee forces and joint disease

Forces transmitted by the knee joint are of great clinical significance. Obesity, which increases the overall magnitude of loads across the knee, is associated with an increased incidence of osteoarthritis, as well as accelerated progression of the disease.[3–8] Forces transmitted across the knee joint during normal walking range between 2 and 3 times body weight ($\times$BW). This is in part owing to the kinetics of acceleration, the high moments generated at the knee, and simultaneous contraction of multiple muscles. Therefore, the net effect of each additional kilogram in body weight is multiplied 2 or 3 times at the knee. Malalignment of the lower extremity, which overloads one compartment at the expense of another, is also associated with progression of osteoarthritis.[9–11] Motion analysis studies, which calculate the external moments of the knee, have correlated an increased peak adduction moment at the knee with pain, radiographic progression, and biomarkers of disease severity.[3,12–15] While these changes in adduction moment are subtle, as little as 3–5° of increased tibial varus alignment can induce a 50% increase in the force transmitted across the medial[16] tibiofemoral compartment

Knee arthroplasty

The only effective treatment for end-stage arthritis is knee arthroplasty. Knee forces are even more important

[1]Shiley Center for Orthopaedic Research and Education at Scripps Clinic, Scripps Health, USA
[2]Department of Mechanical and Aerospace Engineering, University of Florida, USA

Corresponding author:
D D'Lima, Scripps Health, 11025 North Torrey Pines Road, Suite 200, La Jolla, CA 92037, USA.
Email: DLima.Darryl@scrippshealth.org

after arthroplasty because, unlike biological tissues, the materials used in knee replacement do not regenerate or remodel. Knee forces are, therefore, directly implicated in articular wear and damage (especially to the polyethylene component). Contact stresses on the bearing surfaces are a function of the magnitude of contact force, local material properties, and articular conformity.[17] Contact stresses are directly linked to the wear and damage of polyethylene, which is the most common bearing of the tibial articulation.[17–20] Tibiofemoral contact forces are transmitted to the underlying bone. High stresses in the bone, as a result of high tibiofemoral forces or malaligned forces, increase the risk for bone fatigue damage.[16,21] As little as 10–20% change in the mediolateral distribution of axial tibiofemoral load can increase the volume of bone subjected to cyclic strain of greater than 0.4%, which is the threshold for fatigue damage.[16,22]

Calculation and measurement of forces

The computation of knee forces has received much attention. Modeling approaches have varied from two-dimensional (2D) to three-dimensional (3D), with and without the simulation of contact, with and without soft tissues, with and without accounting for muscle cocontraction, and antagonistic effects. The inverse dynamics approach, uses experimentally measured motion analysis and external reaction forces to calculate the forces and moments about the joint.[23] Muscle forces are then derived to balance joint moments and their contribution to total joint forces computed. The forward dynamics approach uses muscle activations and forces to directly predict kinematics, which are then compared with measured kinematics for validation.

The major obstacles to accurate modeling of the knee are:

(a) the complexity of the geometry of the articulating surface;
(b) the multiaxial forces and kinematics;
(c) the importance of passive soft tissues in maintaining stability;
(d) the fact that more than one muscle performs the same action;
(e) the fact that several of the major muscles that act on the knee joint also act on the hip and the ankle;
(f) the complexity of determining the location of the resultant contact force.

Compounding these hurdles is the complexity of analyzing motion, even for a common activity such as walking.

An alternative to computational prediction of knee forces is the direct measurement of knee forces. Advances in smart implant technology and telemetry systems have made measurement possible in vivo in patients receiving total knee arthroplasty. This article is

a concise review of studies that have measured knee forces, the specific goals being to summarize the results, to establish the clinical significance of knee forces, and to suggest future research directions.

Computational prediction of knee forces

A large number of studies have attempted to estimate forces around the knee during various activities. Several approaches have been used to relate knee kinematics and external forces to internal joint contact forces, the most popular being inverse dynamics, forward dynamics, and static body analyses.[24–34] A major challenge for most musculoskeletal joints in general, and the knee in particular, is the problem of redundant muscles, which makes it difficult to find unique solutions for knee forces. Electromyography (EMG)-driven and optimization methods have commonly been used to resolve this issue.[26,34–36]

The diversity of approaches, solution algorithms, and modeling assumptions has led to wide differences in predictions even for the same activities. Among the open kinetic chain activities, isokinetic knee extension has been studied for its relative simplicity for modeling. A 2D static analysis of maximum voluntary isokinetic knee extension with a single quadriceps muscle estimated peak tibiofemoral compressive forces up to $9 \times BW$.[24] At the other end of the spectrum, a 2D inverse dynamics model using a linear optimization algorithm to solve the distribution of synergistic muscle forces estimated peak compressive forces of only $4 \times BW$ during maximal voluntary effort.[25]

Examples of divergent predictions can be found for several activities. When comparing an open kinetic chain with closed kinetic chain knee extension, a static free-body analysis in the sagittal plane predicted maximum compressive forces of $5 \times BW$ during an open kinetic chain extension exercise and $4.5 \times BW$ during a closed kinetic chain extension exercise.[37] On the other hand, a 3D inverse dynamics model utilizing motion analysis, force plates, and EMG (quadriceps, hamstrings, and gastrocnemius) estimated higher knee forces during the closed kinetic chain task (peaking at an average of 6.7 and $6.3 \times BW$ for the squat and leg press, respectively) compared with $5 \times BW$ for open chain knee extension.[26] Peak forces generated during squatting without resistance were estimated at $4.2 \times BW$,[27] while forces calculated at maximum flexion were 2.8 and $3.8 \times BW$ for squatting with heels down and heels up, respectively.[28]

Although walking is a common activity, it is complex to model. The earliest report of predicting forces during walking simplified the problem by grouping muscles based on similar function, which reported peak forces that averaged $3 \times BW$.[29,30] Other reports that grouped muscles with similar function have reported peak forces in the range of 1.7 and $2.4 \times BW$.[31,32] Use of an objective function that minimized total forces and moments

to solve the redundancy problem resulted in peak force predictions approaching $7 \times BW$.[33] Tibiofemoral contact forces were sensitive to the quantities being minimized and varied between 4 to $6 \times BW$ during level walking.[34]

The broad range of differences in estimated peak tibiofemoral contact forces emphasizes the need for experimental validation. All of the above-mentioned studies made several assumptions that have yet to be validated. Anthropometric measurements are particularly important when defining the attachments and wrapping of muscles. Measuring specific attachment points and vectors of action are often challenging. Owing to the large muscle force to moment arm ratios around the knee, small errors in estimated or measured directions of muscle line of action can lead to large differences in estimated moments. An accurate determination of tibiofemoral contact position may also be essential but is difficult to measure. In vivo measurement of tibial compressive forces, therefore, provides an invaluable means of validating such models.

Experimental measurement of knee forces

In vitro: intact knee

Early attempts at measuring tibiofemoral forces in vitro (in cadavers) involved inserting a steel plate between the tibial plateau and the tibial tubercle connected to a vertical intramedullary shaft that was instrumented with strain gauges to measure compressive forces.[38] Predicted knee forces using a 2D static free-body analysis of the loaded knee were within 6% of experimental measurements. Later studies used nested cylinders supporting the transected tibial plateau to measure multiaxial forces and moments in cadavers. These studies reported differences in anteroposterior shear force during a closed chain knee extension with transection of the anterior and posterior cruciate ligaments.[39]

In vitro: knee arthroplasty

Tibiofemoral forces have been measured in vitro after total knee arthroplasty using an instrumented tibial tray. The tibial tray was split into upper and lower halves that were connected by four posts.[40] Strain gauges, below the posts in the lower half, measured compression forces. By monitoring forces in the four quadrants, the total compressive force and center of pressure could be accurately measured, which also yielded the mediolateral distribution of tibiofemoral force. This instrumented tray was coupled with a telemetry system,[41] demonstrating proof of concept that knee forces could be captured wirelessly in vivo.[42] A second-generation tibial tray that could measure all six components of force was later developed.[43]

In vivo

Knee forces in intact normal human knees have yet to be measured in vivo. In canine knees "sensate" scaffolds have been implanted to measure in vivo loads. These are synthetic scaffolds, designed to fill an osteochondral defect, that have been instrumented with strain gauges and a telemetry system to monitor tibiofemoral contact forces in otherwise intact knees.[44,45] In a human subject, a distal femoral tumor replacement prosthesis was instrumented to measure femoral shaft forces in vivo.[46,47] Femoral shaft forces were used to calculate knee forces in the rotating hinged knee component. Peak knee forces reported were $2.8 \times BW$ for walking, $2.8 \times BW$ for stair ascent, $3.1 \times BW$ for stair descent, and $3.6 \times BW$ for jogging.

The first direct measurement of in vivo tibial forces after a primary total knee arthroplasty was in 2004.[48,49] This "first-generation" design measured axial loads at four quadrants of the tibial tray from which the total force and net center of pressure were obtained. A "second-generation" tibial component was later designed and implanted in which all six components of force acting on the tibial tray were measured.[43,50,51] A different six-component knee arthroplasty design was also implanted by the team led by Georg Bergmann.[52,53] In the early postoperative period, peak axial contact forces during walking increased substantially over the first three weeks peaking at $2.8 \times BW$ by the one year follow up.[48,53] Stair descent generated higher forces (3.2–$3.5 \times BW$) than stair ascent (2.9–$3.0 \times BW$). These early results were further substantiated in a cohort of five patients.[54]

Variation of knee forces by activity

Knee forces have been reported in vivo for a variety of activities including recreation and exercise.[51] Peak tibial forces by activity have been summarized in Table 1. Walking on the treadmill at speeds up to 3 miles per hour generated lower peak tibial forces relative to walking on the laboratory floor. Power walking on the treadmill (at 4 miles per hour) generated higher peak tibial forces. Jogging is a high-impact activity that generated peak forces of $3.6 \times BW$ in two subjects implanted with instrumented distal femoral tumor replacement prostheses.[46] In subjects implanted with a primary knee arthroplasty design, jogging generated higher forces, probably owing to more intact musculature around the knee relative to the more extensive tissue resection required for tumor replacement surgery.

Overall, stationary bicycling generated even lower knee forces than walking.[51] Tennis, also considered a high-impact activity, generated high knee forces in the same range as treadmill jogging. The golf swing, although considered a low impact activity, generated high peak tibial forces in the leading knee approaching those of jogging. Elliptical trainers, a low-impact exercise machine, are often recommended for patients who

Table 1. Activities of daily living.

Activity	Peak tibial forces ($\times$ BW)	Notes
Walking[48–51,54]	2.5 – 2.8	Laboratory floor
Treadmill walking[51]	2.1 ± 0.2	1–3 miles per hour
Power walking[51]	2.8 ± 0.4	4 miles per hour on treadmill
Jogging[46]	3.1 – 3.6	Tumor replacement prosthesis
Jogging[51]	4.2 ± 0.2	5 miles per hour on treadmill
Stationary bicycling[51]	1.0 – 1.5	Level 1–5; 60–90 r/min
Golf (lead knee)[51]	4.4 ± 0.1	Left knee in a right-handed golfer
Golf (trailing knee)[51]	3.0 ± 0.2	
Tennis serve[51]	4.2 ± 0.1	
Tennis forehand[51]	4.3 ± 0.4	
Tennis backhand[51]	3.5 ± 0.6	
StairMaster level 1[51]	2.4 ± 0.1	
StairMaster level 3[51]	3.3 ± 0.3	
Elliptical level 1[51]	2.3 ± 0.2	
Elliptical level 11[51]	2.2 ± 0.3	
Leg press[51]	2.8 ± 0.1	Foot reaction force = 1 $\times$ BW
Knee extension[51]	1.5 ± 0.0	Resistance = 0.2 $\times$ BW
Rowing machine[51]	0.9 ± 0.1	

$\times$ BW: times body weight.

experience knee pain during higher impact jogging. Elliptical training generated forces comparable to treadmill walking. Rowing machines, often recommended to increase knee flexion, generated low forces. Both the leg press (against a resistance force equal to body weight) and the squat generated the same peak tibial forces. The leg-press machine can, therefore, be recommended to build up to a squat, if a full weight-bearing squat is not possible.

Given the wide variation in knee forces predicted by computer models for the same activity, it is not surprising that many of these predictions differed from experimental measurements. Mathematical predictions of walking ranged from 1.7 to 7 $\times$ BW[29–34] while experimental measurements were between 2 and 3 $\times$ BW. Predictions of forces for other activities face similar challenges. For example, a closed kinetic chain activity, such as a leg press, is predicted to generate between 4 and 6 $\times$ BW, while that measured in patients averaged less than 3 $\times$ BW. These comparisons do not serve to directly validate the computer models that predicted forces more accurately, since one cannot rule out serendipitous coincidence. For more robust validation, predictions under diverse conditions specifically designed to test major modeling assumptions or simplifications are required. Also, predictions that modeled younger subjects with intact joints cannot be directly compared to older subjects with artificial knee joints. For a more direct and unbiased assessment of modeling methodology, we are hosting an annual open "Grand Challenge Competition to Predict In Vivo Knee Loads". Entire datasets of subject anthropometrics, motion analysis, ground reactions forces, and EMG required for predicting tibiofemoral forces during specific activities are released publicly the preceding year. Experimental measurements of tibiofemoral forces and the accuracy of predictions are only revealed at the Summer Bioengineering Conference of the American Society of Mechanical Engineering (ASME).

Therapeutic modulation of knee forces

Gait modifications

Knee forces have a substantial impact on joint degeneration, injury, and arthritis. The strong link between knee forces and osteoarthritis has led to interest in gait modifications to reduce the medial compartmental force or "offload" the medial compartment. The peak external knee adduction moment has been linked to pain, severity, and rate of progression of arthritis.[12–14,55] Thus, altering the pattern of gait to reduce external adduction moment may "offload" the medial compartment and delay the progression of medial compartmental disease. By monitoring the mediolateral distribution of tibial forces in vivo, a "medial thrust" gait, in which the knee is deliberately medialized, was shown to reduce the external adduction and effectively reduce medial loads on the tibia by 7% to 28%.[56,57]

Walking aids

The use of walking aids such as canes, crutches, or walkers is often recommended to alleviate pain caused by osteoarthritis of the hip and knee. These aids can form an important component of non-pharmacologic and non-surgical treatment. Walking with hiking poles is sometimes recommended to stabilize moments in the frontal plane.[58] Hiking poles can reduce in vivo medial compartmental forces by 15% to 45%.[56] Even more significantly, walking poles reduced the total tibial contact force, presumably owing to partial transfer of ground reaction force to the walking poles.[56]
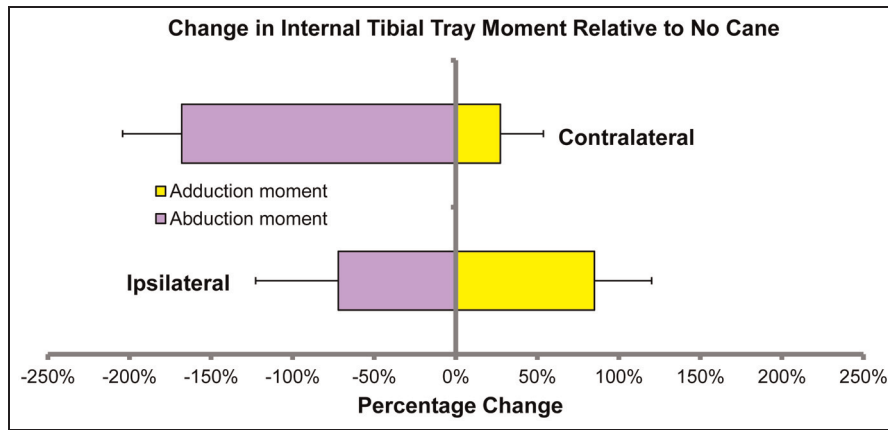
Figure 1. Walking with a cane in the contralateral hand decreased the average peak adduction moment relative to walking without a cane. Walking with a cane in the ipsilateral hand increased the mean peak adduction moment.

A cane is a very convenient walking aid and the efficacy of a cane in reducing hip moments and forces has been documented.[59] A cane reduced peak vertical forces measured using foot pressure sensors.[60] A cane in the contralateral hand resulted in lower shoe forces than one in the ipsilateral hand.[61] Indirect evidence through inverse dynamics analysis suggests that a cane in the contralateral hand reduces external knee adduction moments during gait analysis.[62] We therefore decided to directly measure forces at the knee in vivo to assess the magnitude of any beneficial effect of cane usage.

Tibial forces and moments were recorded in vivo in subjects (N = 3) previously implanted with an instrumented tibial prosthesis[51] while walking with and without a cane. The trials included walking with no cane, walking with a cane in the ipsilateral hand (same side as the implanted knee), and walking with a cane in the contralateral hand (opposite side as the implanted knee). Multiple cycles (10–15 cycles) were averaged into one representative gait cycle for each condition for each subject. Peak tibial axial force and peak adduction and abduction moments on the tibial tray were recorded. The mean peak axial tibial force (F_z) was between 2 and $3 \times$ BW for all the gait conditions and did not appear to change consistently with or without the use of a cane. The mean peak internal abduction moments on the tibial tray were higher (range 0.19% to 1.27% body weight times height [%BW*HT]) when the cane was held in the hand on the same side as the implanted knee when compared with the contralateral side (range 0.02 to 0.96 %BW*HT). The mean peak internal adduction moments on the tibial tray with the cane in the contralateral hand ranged between −0.18 to −0.78 times %BW*HT compared with 0.09 to −0.38 times %BW*HT with the cane in the ipsilateral hand. Walking with a cane in the contralateral hand decreased peak adduction moment by an average of 43% relative to walking without the cane. Walking with a cane in the ipsilateral hand increased the mean peak adduction moment by an average of 9% (Figure 1).

A previous study found differences in external knee moments generated during cane usage in osteoarthritic patients.[62] External knee adduction moments were significantly higher with ipsilateral cane usage relative to unaided gait or contralateral usage. Measurements of adduction moments at the tray are consistent with these results. Proper use of a cane can significantly reduce the adduction moment, which provides biomechanical validation of the use of a walking aid in the conservative management of painful osteoarthritis.

Shoe orthotics

Medial compartmental osteoarthritis has been linked to varus knee alignment and to increased external adduction moment at the knee.[14,15,63,64] Orthotics such as shoe wedges, insoles, and ankle–foot orthoses have been used to alter the mechanical alignment of the knee via the ankle with the objective of reducing the external knee adduction moment.[65] Biomechanically, a laterally based wedge in the sole of the shoe can generate an abduction moment or can reduce the net adduction moment at the knee.[66,67] However, not all studies report successful changes in adduction moment.[65,68] Further, the magnitude of any internal change in in vivo medial joint loading has not been documented. A variable stiffness shoe has been designed that simulates the effect of a dynamic lateral wedge with less subjective discomfort than a static wedge.[69] Since the lateral half of the sole is stiffer than the medial half, the medial sole compresses more on weight bearing, producing a similar effect as a lateral shoe. A variable stiffness shoe reduced the peak external adduction moment of the knee in subjects with medial compartmental osteoarthritis.[70] In a subsequent study, which measured in vivo tibial forces, medial compartment joint contact force was also reduced compared with wearing a shoe without the variable stiffness sole.[71] The change in first peak of the external knee adduction moment was also significantly correlated with the change in first peak of medial contact force. In vivo monitoring of knee forces can, therefore, validate

some of the claims that shoe orthotics can alter the distribution of forces in the knee.

Reduction in ground reaction forces

Lower body-positive pressure chambers have been used as a novel method of reducing net ground reaction forces.[72,73] Placing a treadmill inside a pressurized chamber reduces the effect of gravity during walking. Briefly, the patient is positioned with his or her lower body within the chamber. A neoprene seal at the waist maintains the pressure differential between the lower and upper body. A positive pressure (i.e. higher pressure within the chamber) lifts the patient and reduces the ground reaction force on the treadmill, thus countering the effect of gravity. The pressure can be controlled to generate the desired amount of reduction in ground reaction force. Lower body-positive pressure was effective at reducing ground reaction forces and provided significant postoperative pain relief during ambulation after anterior cruciate reconstruction.[72] Lower body-negative pressure increases the ground reaction forces and has been shown to be effective in countering weightlessness-induced bone loss.[74,75] We monitored knee forces in vivo and compared the reduction in knee forces with the reduction in ground reaction forces.[76] Peak tibial forces correlated with peak ground reaction forces. However, even at pressure settings that reduced ground reaction force to 10%, peak tibial forces remained above $0.5 \times BW$.

Summary of future directions

Experimentally and clinically measured forces provide much needed experimental validation of past and current estimates generated by computer models. Knowledge of forces in the knee provides the clinician with quantitative data to make informed decisions regarding the prevention and treatment of knee injury. Knee forces can also be used to drive computer models that predict outcomes that cannot be readily measured in vivo, such as stress distributions, ligament and muscle forces, wear, damage, and remodeling. Clinical force measurements have been made in a limited number of patients with knee replacements. Extrapolation of these forces to a larger patient population or different age groups has to be validated. We are working to develop a commercially viable instrumented prosthesis. A major challenge is establishing safety across a diverse patient population using a prosthesis with sensors and electronics. Other challenges include developing a low cost, efficient, and durable power source. Remote unsupervised monitoring and continuous data logging are highly attractive but require development of robust data acquisition systems that can be operated by patients and a strategy to manage the bandwidth of real time data as well as the storage and processing of existing data. A major unmet need is measurement of patellofemoral forces. The patellofemoral joint is an important component of the knee and biomechanical dysfunction contributes significantly to disease. Major technological advances are required to measure knee forces in normal intact joints. The current bottlenecks are primarily safety and durability of implantable sensors. Noninvasive methods of measuring forces have yet to be explored, but, if successful, will have a great impact on the field.

References

1. Gray H. *Gray's anatomy: the anatomical basis of clinical practice*. 40th ed. Churchill-Livingstone: Elsevier, 2008.
2. McDermott ID and Amis AA. The consequences of meniscectomy. *J Bone Joint Surg Br* 2006; 88(12): 1549–1556.
3. Amin S, Luepongsak N, McGibbon C A, et al. Knee adduction moment and development of chronic knee pain in elders. *Arthritis Rheum* 2004; 51(3): 371–376.
4. Felson D T, Zhang Y, Hannan M T, et al. Risk factors for incident radiographic knee osteoarthritis in the elderly: the Framingham Study. *Arthritis Rheum* 1997; 40(4): 728–733.
5. Roemer FW, Zhang Y, Niu J, et al. Tibiofemoral joint osteoarthritis: risk factors for MR-depicted fast cartilage loss over a 30-month period in the multicenter osteoarthritis study. *Radiology* 2009; 252(3): 772–780.
6. Felson D T, Anderson JJ, Naimark A, et al. Obesity and knee osteoarthritis. the Framingham Study. *Ann Intern Med* 1988; 109(1): 18–24.
7. Blagojevic M, Jinks C, Jeffery A, et al. Risk factors for onset of osteoarthritis of the knee in older adults: a systematic review and meta-analysis. *Osteoarthritis Cartilage* 2010; 18(1): 24–33.
8. Niu J, Zhang Y Q, Torner J, et al. Is obesity a risk factor for progressive radiographic knee osteoarthritis? *Arthritis Rheum* 2009; 61(3): 329–335.
9. Sharma L, Lou C, Felson DT, et al. Laxity in healthy and osteoarthritic knees. *Arthritis Rheum* 1999; 42(5): 861–870.
10. Sharma L, Song J, Felson DT, et al. The role of knee alignment in disease progression and functional decline in knee osteoarthritis. *JAMA* 2001; 286(2): 188–195.
11. Tanamas S, Hanna FS, Cicuttini FM, et al. Does knee malalignment increase the risk of development and progression of knee osteoarthritis? A systematic review. *Arthritis Rheum* 2009; 61(4): 459–467.
12. Thorp LE, Sumner D R, Wimmer MA, et al. Relationship between pain and medial knee joint loading in mild radiographic knee osteoarthritis. *Arthritis Rheum* 2007; 57(7): 1254–1260.
13. Prodromos CC, Andriacchi TP and Galante JO. A relationship between gait and clinical changes following high tibial osteotomy. *J Bone Joint Surg Am* 1985; 67(8): 1188–1194.
14. Sharma L, Hurwitz DE, Thonar EJ, et al. Knee adduction moment, serum hyaluronan level, and disease

severity in medial tibiofemoral osteoarthritis. *Arthritis Rheum* 1998; 41(7): 1233–1240.

15. Baliunas AJ, Hurwitz DE, Ryals AB, et al. Increased knee joint loads during walking are present in subjects with knee osteoarthritis. *Osteoarthritis Cartilage* 2002; 10(7): 573–579.

16. Wong J, Steklov N, Patil S, et al. Predicting the effect of tray malalignment on risk for bone damage and implant subsidence after total knee arthroplasty. *J Orthop Res* 2010; 29(3): 347–353.

17. D'Lima DD, Chen PC and Colwell C W Jr. Polyethylene contact stresses, articular congruity, and knee alignment. *Clin Orthop Relat Res* 2001; 392: 232–328.

18. Fregly BJ, Sawyer WG, Harman MK, et al. Computational wear prediction of a total knee replacement from in vivo kinematics. *J Biomech* 2005; 38(2): 305–314.

19. McEwen H M, Barnett PI, Bell CJ, et al. The influence of design, materials and kinematics on the in vitro wear of total knee replacements. *J Biomech* 2005; 38(2): 357–365.

20. Knight LA, Pal S, Coleman JC, et al. Comparison of long-term numerical and experimental total knee replacement wear during simulated gait loading. *J Biomech* 2007; 40(7): 1550–1558.

21. Cristofolini L, Affatato S, Erani P, et al. Long-term implant-bone fixation of the femoral component in total knee replacement. *Proc IMechE, Part H: J Engineering in Medicine* 2008; 222(3): 319–331.

22. Pattin CA, Caler WE and Carter DR. Cyclic mechanical property degradation during fatigue loading of cortical bone. *J Biomech* 1996; 29(1): 69–79.

23. Otten E. Inverse and forward dynamics: models of multi-body systems. Philos Trans R *Soc Lond B Biol Sci* 2003; 358(1437): 1493–1500.

24. Nisell R, Ericson MO, Nemeth G, et al. Tibiofemoral joint forces during isokinetic knee extension. *Am J Sports Med* 1989; 17(1): 49–54.

25. Kaufman KR, An KN, Litchy WJ, et al. Dynamic joint forces during knee isokinetic exercise. *Am J Sports Med* 1991; 19(3): 305–316.

26. Wilk KE, Escamilla RF, Fleisig GS, et al. A comparison of tibiofemoral joint forces and electromyographic activity during open and closed kinetic chain exercises. *Am J Sports Med*, 1996; 24(4): 518–527.

27. Shelburne KB and Pandy MG. A dynamic model of the knee and lower limb for simulating rising movements. *Comput Methods Biomech Biomed Engng* 2002; 5(2): 149–159.

28. Smith SM, Cockburn RA, Hemmerich A, et al. Tibiofemoral joint contact forces and knee kinematics during squatting. *Gait & posture* 2008; 27(3): 376–386.

29. Morrison JB. Bioengineering analysis of force actions transmitted by the knee joint. *Biomed Engng* 1968; 3(4): 164–170.

30. Morrison JB. The mechanics of the knee joint in relation to normal walking. *J Biomech* 1970; 3(1): 51–61.

31. Komistek RD, Kane TR, Mahfouz M, et al. Knee mechanics: a review of past and present techniques to determine in vivo loads. *J Biomech* 2005; 38(2): 215–228.

32. Komistek RD, Stiehl JB, Dennis DA, et al. Mathematical model of the lower extremity joint reaction forces using Kane's method of dynamics. *J Biomech* 1998; 31(2): 185–189.

33. Seireg A and Arvikar RJ. The prediction of muscular lad sharing and joint forces in the lower extremities during walking. *J Biomech* 1975; 8(2): 89–102.

34. Collins JJ. The redundant nature of locomotor optimization laws. *J Biomech* 1995; 28(3): 251–267.

35. Lloyd DG and Besier TF. An EMG-driven musculoskeletal model to estimate muscle forces and knee joint moments in vivo. *J Biomech* 2003; 36(6): 765–776.

36. Winby CR, Lloyd DG, Besier TF, et al. Muscle and external load contribution to knee joint contact loads during normal gait. *J Biomech* 2009; 42(14): 2294–2300.

37. Lutz GE, Palmitier RA, An KN, et al. Comparison of tibiofemoral joint forces during open-kinetic-chain and closed-kinetic-chain exercises. *J Bone Joint Surg Am*, 1993; 75(5): 732–739.

38. Perry J, Antonelli D and Ford W. Analysis of knee-joint forces during flexed-knee stance. *J Bone Joint Surg Am* 1975; 57(7): 961–967.

39. Singerman R, Berilla J, Archdeacon M, et al. In vitro forces in the normal and cruciate-deficient knee during simulated squatting motion. *J Biomech Engng* 1999; 121(2): 234–242.

40. Kaufman KR, Kovacevic N, Irby SE, et al. Instrumented implant for measuring tibiofemoral forces. *J Biomech* 1996; 29(5): 667–671.

41. D'Lima DD, Townsend CP, Arms SW, et al. An implantable telemetry device to measure intra-articular tibial forces. *J Biomech* 2005; 38(2): 299–304.

42. Morris BA, D'Lima DD, Slamin J, et al. e-Knee: evolution of the electronic knee prosthesis. Telemetry technology development. *J Bone Joint Surg Am* 2001; 83-A Suppl 2(Pt 1): 62–66.

43. Kirking B, Krevolin J, Townsend C, et al. A multiaxial force-sensing implantable tibial prosthesis. *J Biomech* 2006; 39(9): 1744–1751.

44. Geffre CP, Bliss CL, Szivek JA, et al. Sensate scaffolds coupled to telemetry can monitor in vivo loading from within a joint over extended periods of time. *J Biomed Mater Res B Appl Biomater* 2008; 84(1): 263–270.

45. Szivek JA, Bliss CL, Geffre CP, et al. An instrumented scaffold can monitor loading in the knee joint. *J Biomed Mater Res B Appl Biomater* 2006; 79(2): 218–228.

46. Taylor SJ and Walker PS. Forces and moments telemetered from two distal femoral replacements during various activities. *J Biomech* 2001; 34(7): 839–848.

47. Taylor SJ, Walker PS, Perry JS, et al. The forces in the distal femur and the knee during walking and other activities measured by telemetry. *J Arthroplasty* 1998; 13(4): 428–437.

48. D'Lima DD, Patil S, Steklov N, et al. The Chitranjan Ranawat Award: in vivo knee forces after total knee arthroplasty. *Clin Orthop Relat Res* 2005; 440: 45–49.

49. D'Lima DD, Patil S, Steklov N, et al. Tibial forces measured in vivo after total knee arthroplasty. *J Arthroplasty* 2006; 21(2): 255–262.

50. D'Lima DD, Patil S, Steklov N, et al. In vivo knee moments and shear after total knee arthroplasty. *J Biomech* 2007; 40: S11–S17.

51. D'Lima DD, Steklov N, Patil S, et al. The Mark Coventry Award: in vivo knee forces during recreation and exercise after knee arthroplasty. *Clin Orthop Relat Res* 2008; 466(11): 2605–2611.

52. Heinlein B, Graichen F, Bender A, et al. Design, calibration and pre-clinical testing of an instrumented tibial tray. *J Biomech* 2007; 40 Suppl 1: S4–10.

53. Heinlein B, Kutzner I, Graichen F, et al. ESB Clinical Biomechanics Award 2008: Complete data of total knee replacement loading for level walking and stair climbing measured in vivo with a follow-up of 6–10 months. *Clin Biomech (Bristol, Avon)* 2009; 24(4): 315–326.

54. Kutzner I, Heinlein B, Graichen F, et al. Loading of the knee joint during activities of daily living measured in vivo in five subjects. *J Biomech* 2010; 43(11): 2164–2173.

55. Miyazaki T, Wada M, Kawahara H, et al. Dynamic load at baseline can predict radiographic disease progression in medial compartment knee osteoarthritis. *Ann Rheum Dis* 2002; 61(7): 617–622.

56. Fregly BJ, D'Lima DD and Colwell CW Jr. Effective gait patterns for offloading the medial compartment of the knee. *J Orthop Res* 2009; 27(8): 1016–1021.

57. Fregly BJ, Reinbolt JA, Rooney KL, et al. Design of patient-specific gait modifications for knee osteoarthritis rehabilitation. *IEEE Trans Biomed Engng* 2007; 54(9): 1687–1695.

58. Willson J, Torry MR, Decker MJ, et al. Effects of walking poles on lower extremity gait mechanics. *Med Sci Sports Exerc* 2001; 33(1): 142–147.

59. Ajemian S, Thon D, Clare P, et al. Cane-assisted gait biomechanics and electromyography after total hip arthroplasty. *Arch Phys Med Rehabil* 2004; 85(12): 1966–1971.

60. Aragaki DR, Nasmyth MC, Schultz SC, et al. Immediate effects of contralateral and ipsilateral cane use on normal adult gait. *PM R* 2009; 1(3): 208–213.

61. Edwards BG. Contralateral and ipsilateral cane usage by patients with total knee or hip replacement. *Arch Phys Med Rehabil* 1986; 67(10): 734–740.

62. Chan GN, Smith AW, Kirtley C, et al. Changes in knee moments with contralateral versus ipsilateral cane usage in females with knee osteoarthritis. *Clin Biomech (Bristol, Avon)* 2005; 20(4): 396–404.

63. Andriacchi TP. Dynamics of knee malalignment. *Orthop Clin North Am* 1994; 25(3): 395–403.

64. Mundermann A, Dyrby CO, Hurwitz DE, et al. Potential strategies to reduce medial compartment loading in patients with knee osteoarthritis of varying severity: reduced walking speed. *Arthritis Rheum* 2004; 50(4): 1172–1178.

65. Schmalz T, Blumentritt S, Drewitz H, et al. The influence of sole wedges on frontal plane knee kinetics, in isolation and in combination with representative rigid and semi-rigid ankle-foot-orthoses. *Clin Biomech (Bristol, Avon)* 2006; 21(6): 631–639.

66. Kerrigan DC, Lelas JL, Goggins J, et al. Effectiveness of a lateral-wedge insole on knee varus torque in patients with knee osteoarthritis. *Arch Phys Med Rehabil* 2002; 83(7): 889–893.

67. Crenshaw SJ, Pollo FE and Calton EF. Effects of lateral-wedged insoles on kinetics at the knee. *Clin Orthop Relat Res* 2000; (375): 185–192.

68. Nester CJ, van der Linden ML and Bowker P. Effect of foot orthoses on the kinematics and kinetics of normal walking gait. *Gait & posture* 2003; 17(2): 180–187

69. Fisher DS, Dyrby CO, Mundermann A, et al. In healthy subjects without knee osteoarthritis, the peak knee adduction moment influences the acute effect of shoe interventions designed to reduce medial compartment knee load. *J Orthop Res* 2007; 25(4): 540–546.

70. Erhart JC, Mundermann A, Elspas B, et al. A variable-stiffness shoe lowers the knee adduction moment in subjects with symptoms of medial compartment knee osteoarthritis. *J Biomech* 2008; 41(12): 2720–2725.

71. Erhart JC, Dyrby CO, D'Lima DD, et al. Changes in in vivo knee loading with a variable-stiffness intervention shoe correlate with changes in the knee adduction moment. *J Orthop Res* 2010; 28(12): 1548–1553.

72. Eastlack RK, Hargens AR, Groppo ER, et al. Lower body positive-pressure exercise after knee surgery. *Clin Orthop Relat Res* 2005; (431): 213–219.

73. Cutuk A, Groppo ER, Quigley EJ, et al. Ambulation in simulated fractional gravity using lower body positive pressure: cardiovascular safety and gait analyses. *J Appl Physiol* 2006; 101(3): 771–777.

74. Smith SM, Davis-Street JE, Fesperman JV, et al. Evaluation of treadmill exercise in a lower body negative pressure chamber as a countermeasure for weightlessness-induced bone loss: a bed rest study with identical twins. *J Bone Miner Res* 2003; 18(12): 2223–2230.

75. Zwart SR, Hargens AR, Lee SM, et al. Lower body negative pressure treadmill exercise as a countermeasure for bed rest-induced bone loss in female identical twins. *Bone* 2007; 40(2): 529–537.

76. Macias BR, D'Lima DD, Patil SP, et al. In vivo knee forces during lower body positive pressure treadmill exercise at various body weight levels. *ORS Trans* 2007; 32: 1849.